

NOISE

- * Any unwanted signal is considered as noise.
- * Noise tends to **interfere** with received or produced signals.
- * **EXAMPLES** ∴
 - * In receivers, several electrical **disturbances** produces noise and thus modifying the required signal in an unwanted form.
 - * **Radio Receivers**: The loudspeaker produce a hiss type sound due to noise.
 - * **T. V.** ∴ The noise can be seen as snow in the displaying screen.
 - * In pulse communication: The noise may alter the pulse from $+2\ell$ to -2ℓ .

Thus The noise may limit the performance of a communication system.

* Generally speaking: There are External & Internal noises.

* External noise: Atmospheric noise,

External noise is that noise generated outside the communication system.

Extraterrestrial noise,

Industrial noise

Shot noise,

* Internal noise:

Internal noise is that noise which is generated inside a communication system

Partition noise,

Low frequency or Flicker noise.

High frequency or transit-time noise,

Thermal noise.

Atmospheric Noise

- * Atmospheric noise also called static noise.
- * Static noise produced by discharges in thunderstorms and other natural electrical disturbances of the atmosphere.
- * It is electrical impulses & random in nature.
- * Atmospheric noise distributed over the complete frequency spectrum used for radio communication.
- *
$$\text{atmospheric noise strength} \propto \frac{1}{\text{frequency}}$$
- * Large atmospheric noise is produced in Low & Medium frequency bands.
- * Very small noise is produced in VHF & UHF bands.
- * Atmospheric noise becomes less severe when $F > 30 \text{ MHz}$.

Extraterrestrial Noise : خارج الارض

* Extraterrestrial noise also called **space noise**.

* Extraterrestrial noise $\left\{ \begin{array}{l} \text{Solar noise} \\ \text{Cosmic noise} \end{array} \right.$

* **Solar noise** :- emanating from sun.

* **Cosmic noise** :- emanating from distant stars and galaxies.

* cosmic noise also called **space noise**.

* cosmic noise is **significant at $F = 1.43 \text{ GHz}$** .

* However, cosmic noise exists in the range **$15 \text{ MHz} - 100 \text{ GHz}$** .

Industrial Noise : (Manmade Noise)

* **Industrial or manmade noise is due to :-**

* Automobile & aircraft ignition,

* electrical motors,

* switch gears and leakage from high voltage transmission lines

* other heavy electrical equipments.

* Manmade noise extending in the range **$1 \text{ MHz} - 600 \text{ MHz}$** .

Shot Noise :-

* Arises in active devices due to random behaviour of charge carriers.

- Electron tubes,
- Semiconductor devices
- Solid state devices

* Shot noise current is given by

$$i(t) = I_0 + i_n(t)$$

where I_0 is the mean (constant) and $i_n(t)$ is the shot (fluctuating) noise.

* $i_n(t)$ is random (indeterministic), therefore it can be specified by its power density spectrum.

* Power density spectrum of $i_n(t)$ is

$$i_n(t) \xleftrightarrow{\text{F.T.}} S_{i_n}(\omega) = q I_0$$

where q is electronic charge, and I_0 is the mean value.

* The transit time of an electron in a diode is

$$\tau = 3.36 * \frac{d}{\sqrt{V}} \text{ } \mu\text{second}$$

d = distance between cathode and anode
 V = Voltage across diode.

Partition Noise %

- * generated in a circuit when a current has to divide between two or more paths.
- * Hence, diode less noise than a BJT transistor.
- * Metal-Oxide Semiconductor Field Effect Transistor
MOSFET transistor less noise than BJT transistor because the gate draws zero current.
- * Therefore, MOSFET used in low noise microwave amplification.

Flicker Noise :-

* also called Low-frequency noise

* also known as $1/f$ noise

* power spectral density inversally proportional to the frequency.

$$F \propto \frac{1}{S(\omega)}$$

- As Frequency decreases \rightarrow noise increases.
- As Frequency increases \rightarrow noise decreases.

* Flicker noise generated from fluctuation in the carrier density.

Transit-Time noise :-

* Also called High-frequency noise.

* Generated when charge-carriers crossing a junction.

* Some charge-carriers diffuse back to the source.

* When diffusing back, input admittance increases.

* power spectral density $\propto F$.

Thermal Noise ∴ ∴

* Also called as ∴ ∴

(i) White noise,

(ii) Johnson noise,

(iii) KTB noise

* Generated randomly in a resistor or resistive components of complex impedances due to rapid and random motion of the molecules, atoms and electrons.

* Maximum noise power of a resistor is :-

$$P_n \propto T \cdot B$$

or

$$P_n = k \cdot T \cdot B$$

where

k = Boltzmann's constant = 1.38×10^{-23} J/deg.K

T = Absolute temperature = (ambient temperature + 273) °K

B = Bandwidth of operation in Hz

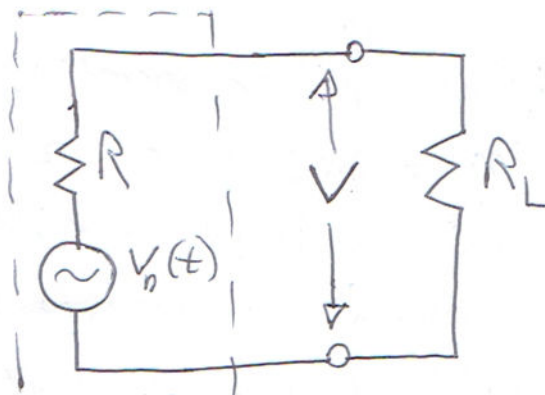
Noisy Resistor

* Thermal or Johnson or white noise generated in a noisy resistor is **random and has zero average (dc) value.**

* If a very sensitive AC-Voltmeter connected across a resistor in temperature of 27°C (room temperature = $27^{\circ}\text{C} + 273 = 300^{\circ}\text{K}$), **then**

*** Some rms voltage can be captured, this is the noise voltage.**

* Voltage model of a noisy resistor \longrightarrow



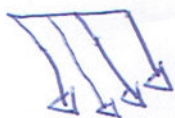
* According to maximum power transfer theorem:-

$$R_2 = R$$

$$P_n = \frac{V^2}{R}$$

* using voltage divider rule : $V = \frac{V_n}{2}$

$$P_n = \frac{V_n^2}{4R}$$



* Since $P_n = kTB$

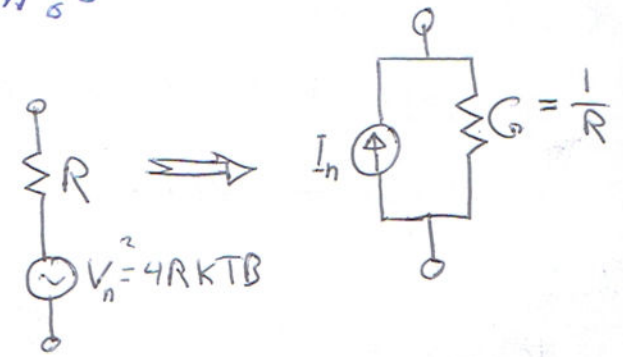
$V_n = \sqrt{4RkTB}$

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* Using Norton's Theorem:

and let $G = \frac{1}{R}$

$I_n = \sqrt{4GkTB}$



EX. 1: An amplifier operating over the frequency range 18-20 MHz has a 10 kΩ input resistor. Calculate the rms noise voltage at the input to this amplifier if the ambient temperature is 27°C.

Solution: Boltzmann's constant $k = 1.38 \times 10^{-23}$ J/degK

$R = 10 \text{ k}\Omega$

$T = 27 + 273 = 300 \text{ K}$

Bandwidth $B = 20 - 18 = 2 \text{ MHz}$

$V_n = \sqrt{4RkTB} = \sqrt{4 \times 10000 \times 1.38 \times 10^{-23} \times 300 \times 2 \times 10^6}$

$= \sqrt{8 \times 10^{10} \times 300 \times 1.38 \times 10^{-23}}$

$\approx 18.199 \mu \text{ Volts}$

EX. 2

Calculate the rms noise voltage at the input of a video amplifier using a device having $300\ \Omega$ equivalent noise resistance and $400\ \Omega$ input resistance. It is given that the bandwidth of the amplifier is $7\ \text{MHz}$ and the ambient temperature is 27°C . Note that the two resistors are connected in series.

Solution $T = 27^\circ\text{C} + 273 = 300^\circ\text{K}$.

$$R_{\text{series}} = R_S = R_1 + R_2 = 700\ \Omega$$

$$B = 7 \times 10^6\ \text{Hz}$$

$$V_{n_z} = \sqrt{4R_S K T B} = \sqrt{4 \times 700 \times 1.38 \times 10^{-23} \times 300 \times 7 \times 10^6}$$

$$V_{n_z} \cong 9\ \mu\text{V}$$

EX. 3 Two resistors of $20\ \text{k}\Omega$ and $50\ \text{k}\Omega$ are connected in parallel when the room temperature was 15°C or $290\ \text{K}$. For a given bandwidth of $100\ \text{kHz}$, determine the thermal noise voltage generated by: (a) each resistor (b) the two resistors in parallel.

Solution: (a) $V_{n_1} = \sqrt{4 \times 20 \times 10^3 \times 1.38 \times 10^{-23} \times 290 \times 100 \times 10^3} \cong 5.66\ \mu\text{V}$.

$$V_{n_2} = \sqrt{4 \times 50 \times 10^3 \times 1.38 \times 10^{-23} \times 290 \times 100 \times 10^3} \cong 8.95\ \mu\text{V}$$

(b) in parallel $R_{\text{parallel}} = R_p \cong 14.2857\ \text{k}\Omega$.

$$V_{n_p} = \sqrt{4 \times 14.2857 \times 10^3 \times 1.38 \times 10^{-23} \times 290 \times 100 \times 10^3}$$

$$V_{n_p} \cong 4.78\ \mu\text{V}$$

EX. What will be the thermal noise power density of a resistor in room temperature $T = 290$ K under maximum power transfer conditions?

Solution $T = 290$ K

$$P_n = 4RKT B \quad \left. \begin{array}{l} \text{under maximum power transfer} \\ \text{should divide by } 4R. \end{array} \right\}$$

$$\frac{P_n}{4RB} = KT = 4.002 \times 10^{-21} \frac{W}{Hz}$$



* For communication system analysis, power ratio in decibels (dB) is usually used.

$$* 1 \text{ watt} = 10 \log_{10} \left(\frac{P_{\text{watts}}}{1 \text{ watt}} \right)$$

$$= 10 \log_{10} \left(\frac{1}{1} \right) = 10 \log_{10} (1)$$

$$= 0 \text{ dBW}$$

$$* 1 \text{ mwatt} = 10 \log_{10} \left(\frac{P_{\text{mwatt}}}{1 \text{ mW}} \right)$$

$$= 10 \log_{10} \left(\frac{1 \text{ mW}}{1 \text{ mW}} \right)$$

$$= 10 \log_{10} (1)$$

$$= 0 \text{ dBm}$$

$$* \text{EX. } 13 \text{ W} = 10 \log_{10} \left(\frac{13 \text{ W}}{1 \text{ W}} \right) = 10 \log_{10} (13) \approx 11.14 \text{ dBW}$$

$$50 \text{ mW} = 10 \log_{10} \left(\frac{50 \text{ mW}}{1 \text{ mW}} \right) = 10 \log_{10} (50) \approx 17 \text{ dBm}$$

$$13 \text{ W} = 10 \log_{10} \left(\frac{13000 \text{ mW}}{1 \text{ mW}} \right) = 10 \log_{10} (13000) \approx 41.14 \text{ dBm}$$

Signal-to-Noise Ratio: (SNR)

* The ratio of **Signal power** to the **Noise power** at the same band of frequency is called **Signal-to-Noise Ratio (SNR)** or **(S/N)**.

$$\frac{S}{N} = \frac{\text{Signal power}}{\text{Noise power}} = \frac{\text{Power spectrum density of signal}}{\text{Power spectrum density of noise}}$$

Noise Factor

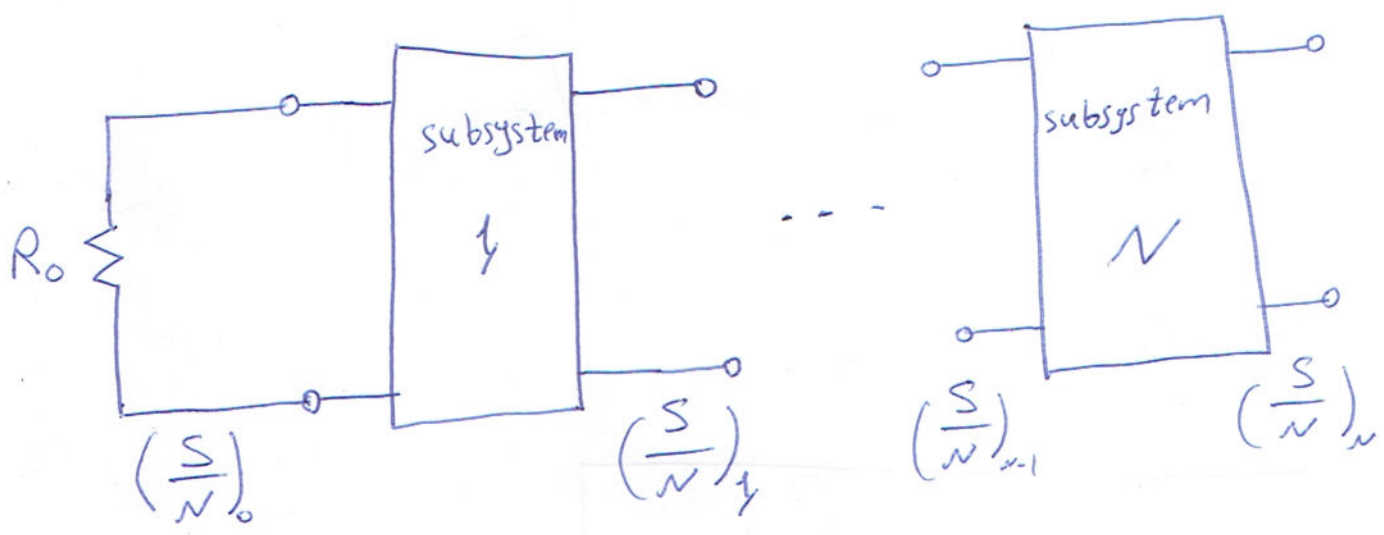
* Also called noise Figure

* Noise Figure is defined as:-

$$NF = \frac{\text{Input SNR}}{\text{output SNR}} = \frac{SNR_i}{SNR_o}$$

* Systems are usually represented as subsystems connected in cascade form.

* Assuming output impedance of a certain system is equal to the input impedance of the next system. (usually 50-Ω).



* Now, For the l^{th} subsystem, noise figure F_l is

$$\left(\frac{S}{N}\right)_l = \frac{1}{F_l} \left(\frac{S}{N}\right)_{l-1}$$

* Assuming that the l^{th} subsystem has gain G_a , then

$$P_{nl} = G_a P_{nl-1} \quad \text{Assuming the system is linear}$$



$$\therefore \left(\frac{S}{N}\right)_l = \frac{1}{F_l} \left(\frac{S}{N}\right)_{l-1}$$

and

$$F_l = \frac{P_{n,l}}{G_a P_{n,l-1}} = \frac{P_{n,l}}{G_a K T B}$$

* considering the internal power $P_{int,l}$

$$P_{n,l} = G_a P_{n,l-1} + P_{int,l}$$

$$\therefore F_l = 1 + \frac{P_{int,l}}{G_a K T B}$$

Noise Temperature \therefore

* Equivalent Noise Temperature of a system is:-

$$T_n = \frac{P_{n,max}}{K B}$$

* $P_{n,max}$ is the maximum noise power of the source into bandwidth B .

Effective Noise Temperature

* effective noise temperature of subsystem l is

$$T_e = \frac{P_{int,l}}{G_a K B}$$

$$F_l = 1 + \frac{P_{int,l}}{G_a K T_0 B} = 1 + \frac{T_e}{T_0}$$

where $T_0 = 290 \text{ K} = T + 273^\circ$

* We can express $P_{n,l}$ as

$$P_{n,l} = G_a K B (T_e + T)$$

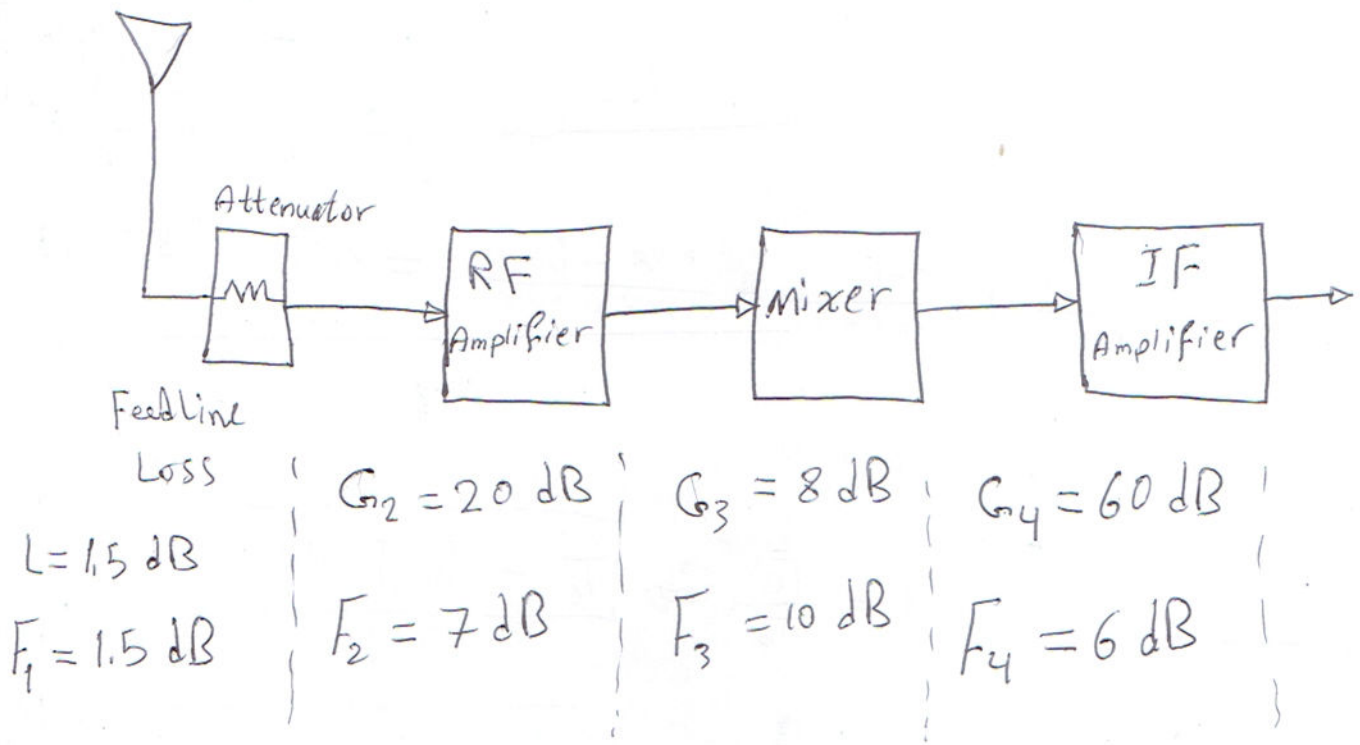
* In general for an arbitrary number of stages of subsystems (Friis's Formula)

$$F = F_1 + \frac{F_2 - 1}{G_{a1}} + \frac{F_3 - 1}{G_{a1} G_{a2}} + \frac{F_4 - 1}{G_{a1} G_{a2} G_{a3}} \dots$$

$$T_e = T_{e1} + \frac{T_{e2}}{G_{a1}} + \frac{T_{e3}}{G_{a1} G_{a2}} + \frac{T_{e4}}{G_{a1} G_{a2} G_{a3}} \dots$$

* An attenuator of x dB means an attenuator has a noise figure of $-x$ dB.

EX. 1 For a receiver system, the antenna was connected to an RF-amplifier with feedline loss of 1.5 dB. The RF-amplifier has gain = 20 dB and noise factor of 7 dB. The RF-amplifier has been connected to a mixer of gain = 8 dB and noise figure = 10 dB, the IF-amplifier was connected to the output of the mixer, where the IF-amplifier has gain = 60 dB and noise figure = 6 dB. Calculate the system noise figure and the system's effective temperature at 290 K.



Solution

$$G_1 = 1.5 \text{ dB}, G_2 = 20 \text{ dB}, G_3 = 8 \text{ dB}, G_4 = 60 \text{ dB}.$$

$$F_1 = 1.5 \text{ dB}, F_2 = 7 \text{ dB}, F_3 = 10 \text{ dB}, F_4 = 6 \text{ dB}.$$

$$G_{\text{dB}} = 10 \log_{10} G \Rightarrow \log_{10} G = \frac{G_{\text{dB}}}{10} \Rightarrow \boxed{G = 10^{\frac{G_{\text{dB}}}{10}}}$$

* we have $G_1 = L = \text{losses} = 1.5 \text{ dB}$, hence it is $\boxed{-1.5 \text{ dB}}$

$G_1 = 10^{-\frac{1.5}{10}} = 0.70795$		$F_1 = 10^{\frac{1.5}{10}} = 1.41$
$G_2 = 10^{\frac{20}{10}} = 100$		$F_2 = 10^{\frac{7}{10}} = 5.01$
$G_3 = 10^{\frac{8}{10}} = 6.3$		$F_3 = 10^{\frac{10}{10}} = 10$
$G_4 = 10^{\frac{60}{10}} = 10^6 = 1000000$		$F_4 = 10^{\frac{6}{10}} = 3.98$

The system noise figure is

$$F = 1.41 + \frac{5.01-1}{0.707} + \frac{10-1}{0.707 \times 100} + \frac{3.98-1}{0.707 \times 100 \times 6.3} = 7.19 \text{ or } 8.57 \text{ dB}$$

The effective noise temperature is

$$F = \frac{T_e}{T_0} + 1 \Rightarrow F - 1 = \frac{T_e}{T_0} \Rightarrow \boxed{T_e = T_0 (F - 1)}$$

$$\therefore T_e = 290(7.19 - 1) = 1796.3 \text{ K}.$$

Comments and enhancements on Ex. 1, pages [197-198].

* To reduce the noise figure (to improve system performance), interchange the cable and RF pre-amplifier.

* In practice this may mean locating an RF preamplifier on back of the receive antenna, as in a satellite TV receiver

$$F = 5.04 - \frac{1.41-1}{100} + \frac{10-1}{100 \times 0.707} + \frac{3.98-1}{100 \times 0.707 \times 6.3} = 5.15 \text{ or } 7.12 \text{ dB}$$

$$T_e = 1202.9 \text{ K}$$

* Going back to the original example, let the antenna, suppose the antenna has an effective noise temperature of $T_s = 400 \text{ K}$ and the system bandwidth $B = 100 \text{ kHz}$. What is the maximum available output noise power in dBm?

$$P_n = G_a k B (T_s + T_e) \Rightarrow G_a = -1.5 + 20 + 8 + 60 = 86.5 \text{ dB}$$

$$kT_0 = -174 \text{ dBm/Hz}, T_0 = 290 \text{ K}$$



$$P_n = 86.5 - 174 + 10 \log_{10} \left(\frac{400 + 1796.3}{290} \right) + 10 \log_{10} 10^5$$
$$= -28.71 \text{ dBm}$$

* what will be the received signal power at the antenna terminals for a system output SNR of 20dB?

$$10 \log_{10} \left(\frac{G_a P_r}{P_n} \right) = 20$$

$$\begin{aligned} P_{r \text{ dB}} &= 20 + P_{n \text{ dB}} - G_a \text{ dB} \\ &= 20 + (-28.71) - 86.5 \\ &= -95.21 \text{ dBm} \end{aligned}$$