

Time - Domain Analysis of control system

The time response of a control system consists of two parts: the transient response and the steady-state response. By transient response, we mean that which goes from the initial state to the final state. By steady-state response, we mean the manner in which the system output behaves as (t) approaches infinity. Thus the system response $c(t)$ may be written as

$$c(t) = C_{tr}(t) + C_{ss}(t)$$

where

$C_{tr}(t)$ ---- transient response.

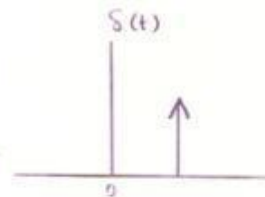
$C_{ss}(t)$ ---- steady-state response.

The typical test signals for the time response of control system are:

① - Unit Impulse Response: $S(s) = 1$

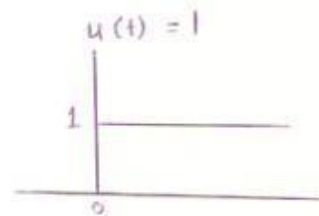
the time response is the inverse Laplace transform of $G(s)$

$$y(t) = \mathcal{L}^{-1} G(s)$$



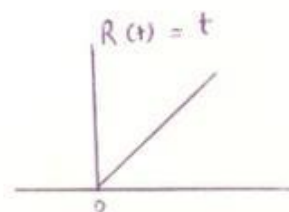
② - Unit step input: $U(s) = \frac{1}{s}$

$$y(t) = \mathcal{L}^{-1} G(s) \cdot U(s)$$



③ - Ramp input: $R(s) = \frac{1}{s^2}$

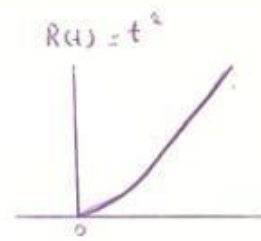
$$y(t) = \mathcal{L}^{-1} G(s) \cdot R(s)$$



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④ - Parabolic input : $R(s) = \frac{1}{s^3}$

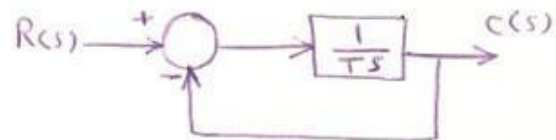
$$y(t) = \int^{-1} G(s) \cdot R(s)$$



Transient Response

① - Transient Response of first order system :-

$$\frac{C(s)}{R(s)} = \frac{1}{1+Ts}$$



First order system.

(a) Unit-step Response : $R(s) = \frac{1}{s}$

$$C(s) = \frac{1}{Ts+1} \cdot \frac{1}{s}$$

By using partial fraction gives

$$C(s) = \frac{1}{s} - \frac{T}{Ts+1} = \frac{1}{s} - \frac{1}{s+(\frac{1}{T})}$$

Taking the inverse Laplace transform gives

$$c(t) = 1 - e^{-(t/T)} \quad \text{for } t \geq 0$$

Notes :

- $c(t)$ initially zero and finally one.
- At $t = T$, the value of $c(t)$ is 0.632 or $c(t)$ reach 63.2% of its final value, where T is time constant of the system.
- The exponential response curve is that the slope of the tangent line at $t=0$ is $1/T$.
 $\frac{dc}{dt} \Big|_{t=0} = \frac{1}{T} e^{-(t/T)} \Big|_{t=0} = 1/T$

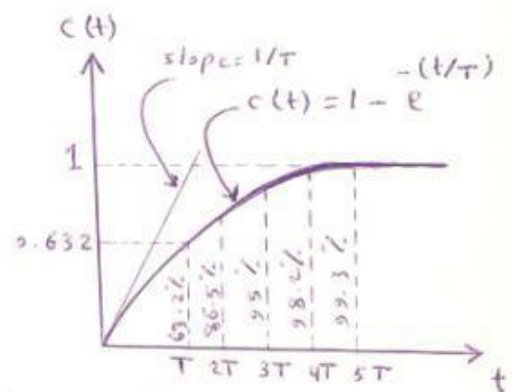


Fig. Exponential response curve

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(b) Unit-Ramp Response: $R(s) = \frac{1}{s^2}$

$$C(s) = \frac{1}{Ts+1} \cdot \frac{1}{s^2}$$

by partial fraction gives

$$C(s) = \frac{1}{s^2} - \frac{T}{s} + \frac{T^2}{Ts+1}$$

taking ^{inverse} Laplace transform, we obtain

$$c(t) = t - T + T e^{-t/T}, \text{ for } t \geq 0$$

The error signal $e(t)$ is then

$$e(t) = r(t) - c(t) = T(1 - e^{-t/T})$$

$$e(\infty) = T$$

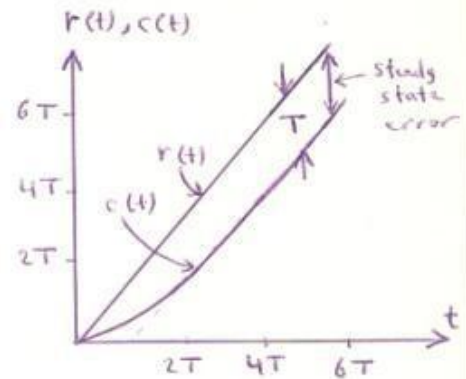


Fig. Unit-ramp response

(c) Unit-Impulse Response: $R(s) = 1$

$$C(s) = \frac{1}{Ts+1}$$

The inverse Laplace transform gives

$$c(t) = \frac{1}{T} e^{-t/T}, \text{ for } t \geq 0$$

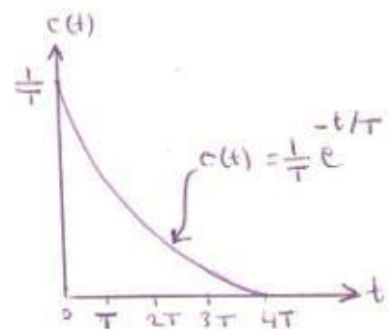


Fig. Unit-impulse response

② - Transient Response of second order system:-

For servo system

$$J\ddot{c} + B\dot{c} = T$$

$$J s^2 c(s) + B s c(s) = T c(s)$$

$$\frac{c(s)}{T c(s)} = \frac{1}{s(Js+B)}$$

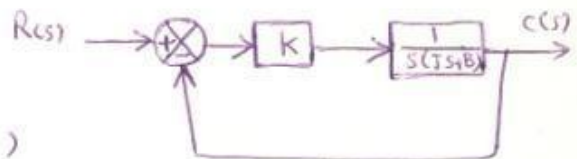


Fig. Servo system

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The closed-loop transfer function is then obtained as

$$\frac{C(s)}{R(s)} = \frac{K}{Js^2 + Bs + K} = \frac{(K/J)}{s^2 + (B/J)s + (K/J)}$$

This T-F can be rewritten as

$$\frac{C(s)}{R(s)} = \frac{K/J}{\left[s + \frac{B}{2J} + \sqrt{\left(\frac{B}{2J}\right)^2 - \frac{K}{J}} \right] \left[s + \frac{B}{2J} - \sqrt{\left(\frac{B}{2J}\right)^2 - \frac{K}{J}} \right]}$$

The closed-loop poles are complex conjugates if $B^2 - 4JK < 0$ and they are real if $B^2 - 4JK \geq 0$.

In transient response analysis, it is convenient to write

$$\frac{K}{J} = \omega_n^2, \quad \frac{B}{J} = 2 \zeta \omega_n = 2\sigma$$

where σ -- is called the attenuation

ω_n -- the undamped natural frequency

ζ -- the damping ratio.

The damping ratio (ζ) is the ratio of the actual damping (B) to the critical damping $B_c = 2\sqrt{JK}$

$$\zeta = \frac{B}{B_c} = \frac{B}{2\sqrt{JK}}$$

hence, the T-F can be written as

$$\frac{C(s)}{R(s)} = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

This form is called the standard form of the second-order system.

The dynamic behavior of the second-order system can then be described in terms of two parameters ζ and ω_n . If $0 < \zeta < 1$, the closed-loop poles are complex conjugates and lie in the left-half s -plane.

The system is then called underdamped, and the transient response is oscillatory. If $\zeta = 0$, the transient response does not die out. If $\zeta = 1$, the system is called critically damped. Overdamped systems correspond to $\zeta > 1$.

We shall now solve for the response of the second order system (servo system) to a unit-step input for three cases: the underdamped ($0 < \zeta < 1$), critically ($\zeta = 1$), and overdamped ($\zeta > 1$).

(a) Underdamped case ($0 < \zeta < 1$):

In this case, $\frac{C(s)}{R(s)}$ can be written as

$$\frac{C(s)}{R(s)} = \frac{\omega_n^2}{(s + \zeta\omega_n + j\omega_d)(s + \zeta\omega_n - j\omega_d)}$$

where

$\omega_d = \omega_n \sqrt{1 - \zeta^2}$. The frequency ω_d is called damped natural frequency.

For a unit-step input, $C(t)$ can be written

$$C(s) = \frac{\omega_n^2}{(s^2 + 2\zeta\omega_n s + \omega_n^2) s}$$

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$$C(s) = \frac{1}{s} - \frac{s + 2\frac{1}{2}\omega_n}{s^2 + 2\frac{1}{2}\omega_n s + \omega_n^2}$$

$$= \frac{1}{s} - \frac{s + \frac{1}{2}\omega_n}{(s + \frac{1}{2}\omega_n)^2 + \omega_d^2} - \frac{\frac{1}{2}\omega_n}{(s + \frac{1}{2}\omega_n)^2 + \omega_d^2}$$

inverse
In \uparrow Laplace transform:

$$\mathcal{L}^{-1} \left[\frac{s + \frac{1}{2}\omega_n}{(s + \frac{1}{2}\omega_n)^2 + \omega_d^2} \right] = e^{-\frac{1}{2}\omega_n t} \cos \omega_d t$$

$$\mathcal{L}^{-1} \left[\frac{\omega_d}{(s + \frac{1}{2}\omega_n)^2 + \omega_d^2} \right] = e^{-\frac{1}{2}\omega_n t} \sin \omega_d t$$

hence, $\mathcal{L}^{-1}[C(s)] = c(t)$

$$\therefore c(t) = 1 - e^{-\frac{1}{2}\omega_n t} \left(\cos \omega_d t + \frac{\frac{1}{2}\omega_n}{\sqrt{1 - \frac{1}{4}}} \sin \omega_d t \right)$$

$$= \frac{e^{-\frac{1}{2}\omega_n t}}{\sqrt{1 - \frac{1}{4}}} \sin \left(\omega_d t + \tan^{-1} \frac{\sqrt{1 - \frac{1}{4}}}{\frac{1}{2}} \right), \text{ for } t \geq 0$$

$$c(t) = r(t) - c(t)$$

$$= e^{-\frac{1}{2}\omega_n t} \left(\cos \omega_d t + \frac{\frac{1}{2}\omega_n}{\sqrt{1 - \frac{1}{4}}} \sin \omega_d t \right), \text{ for } t \geq 0$$

If $\frac{1}{2} = 0$,

$$c(t) = 1 - \cos \omega_n t, \text{ for } t \geq 0$$

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(b) Critically damped case ($\zeta = 1$):

If the two poles of $\frac{C(s)}{R(s)}$ are equal, the system is said to be a critically damped one.

For a unit-step input, $R(s) = \frac{1}{s}$ and $C(s)$ can be written

$$C(s) = \frac{\omega_n^2}{(s + \omega_n)^2 s}$$

Taking inverse Laplace transform gives

$$c(t) = 1 - e^{-\omega_n t} (1 + \omega_n t), \text{ for } t \geq 0$$

(c) Overdamped case ($\zeta > 1$):

In this case, the two poles of $\frac{C(s)}{R(s)}$ are negative real and unequal.

For a unit-step input, $R(s) = \frac{1}{s}$ and $C(s)$ can be written

$$C(s) = \frac{\omega_n^2}{(s + \frac{1}{2}\omega_n + \omega_n\sqrt{\zeta^2 - 1})(s + \frac{1}{2}\omega_n - \omega_n\sqrt{\zeta^2 - 1})s}$$

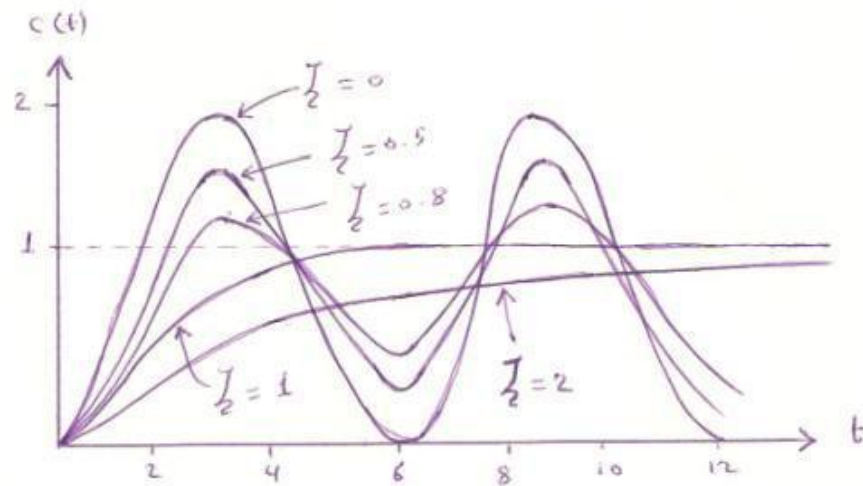
The inverse Laplace transform for above T.F is

$$\begin{aligned} c(t) &= 1 + \frac{1}{2\sqrt{\zeta^2 - 1} (\frac{1}{2} + \sqrt{\zeta^2 - 1})} e^{-(\frac{1}{2} + \sqrt{\zeta^2 - 1})\omega_n t} \\ &\quad - \frac{1}{2\sqrt{\zeta^2 - 1} (\frac{1}{2} - \sqrt{\zeta^2 - 1})} e^{-(\frac{1}{2} - \sqrt{\zeta^2 - 1})\omega_n t} \\ &= 1 + \frac{\omega_n}{2\sqrt{\zeta^2 - 1}} \left(\frac{e^{-s_1 t}}{s_1} - \frac{e^{-s_2 t}}{s_2} \right), \text{ for } t \geq 0 \end{aligned}$$

where $s_1 = (\frac{1}{2} + \sqrt{\zeta^2 - 1})\omega_n$ and $s_2 = (\frac{1}{2} - \sqrt{\zeta^2 - 1})\omega_n$

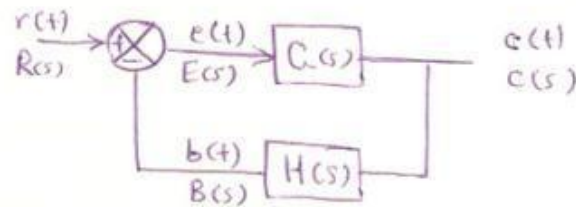
Thus, the response $c(t)$ includes two decaying exponential terms.

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Steady-state Error

The steady-state error is a measure of accuracy and in designed problem one of the objectives is to keep this error to minimum value.



$$e(t) = r(t) - b(t)$$

$$\begin{aligned} E(s) &= R(s) - B(s) = R(s) - H(s)C(s) \\ &= R(s) - H(s)C(s)E(s) \end{aligned}$$

$$E(s) = \frac{R(s)}{1 + C(s)H(s)}$$

$$\text{steady-state error} = E_{ss} = \lim_{t \rightarrow \infty} e(t)$$

using final value theorem, E_{ss} is

$$\lim_{t \rightarrow \infty} e(t) = \lim_{s \rightarrow 0} s \cdot F(s) = \lim_{s \rightarrow 0} \frac{s R(s)}{1 + C(s)H(s)}$$