

(41)

### Types of Control system :

In general  $G(s) H(s)$  may be written as

$$G(s) H(s) = \frac{K(1+T_1 s)(1+T_2 s) \dots (1+T_m s)}{s^J (1+T_{a1} s)(1+T_{a2} s) \dots (1+T_{an} s)}$$

where  $K, T_{i,j}$  are constants

$J$  ---- type of the system

$$J = 0 \Rightarrow \text{type 0}$$

$$J = 1 \Rightarrow \text{type 1}$$

$$J = 2 \Rightarrow \text{type 2}$$

Ex:

$$G(s) H(s) = \frac{K(s+1)}{(s+2)(s+6)} \Rightarrow \text{type 0}$$

$$G(s) H(s) = \frac{K}{(s^2 + 2s)} \Rightarrow \text{type 1}$$

### static Position Error Constant $K_p$ :

The steady-state error of the system for a unit-step input is:

$$e_{ss} = \lim_{s \rightarrow 0} \frac{s}{1 + G(s) H(s)} \cdot \frac{1}{s} = \frac{1}{1 + \lim_{s \rightarrow 0} G(s) H(s)}$$

The static position error constant  $K_p$  is defined by

$$K_p = \lim_{s \rightarrow 0} G(s) H(s)$$

$$\therefore e_{ss} = \frac{1}{1 + K_p}$$

for type 0 system

$$K_p = \lim_{s \rightarrow 0} \frac{K(1+T_1 s)(1+T_2 s) \dots}{(1+T_{a1} s)(1+T_{a2} s) \dots} = K$$

(42)

For a type 1 or higher system

$$K_p = \lim_{s \rightarrow 0} \frac{K(1+T_1s)(1+T_2s) \dots}{s^J(1+T_{as})(1+T_{bs}) \dots} = \infty, \text{ for } J \geq 1$$

$$\therefore e_{ss} = \frac{1}{1+K} \quad \text{for type 0 systems}$$

$$e_{ss} = 0 \quad \text{for type 1 or higher systems}$$

### static velocity Error Constant K\_v :

The steady-state error of the system with a unit ramp input is given by

$$e_{ss} = \lim_{s \rightarrow 0} \frac{s}{1+C(s)H(s)} \cdot \frac{1}{s^2} = \lim_{s \rightarrow 0} \frac{1}{s + S C(s) H(s)}$$

$$e_{ss} = \lim_{s \rightarrow 0} \frac{1}{S C(s) H(s)}$$

The static Velocity error constant  $K_v$  is defined by

$$K_v = \lim_{s \rightarrow 0} s C(s) H(s)$$

$$\therefore e_{ss} = \frac{1}{K_v}$$

$$\text{For a type 0 system, } K_v = \lim_{s \rightarrow 0} \frac{sK(1+T_1s)(1+T_2s) \dots}{(1+T_{as})(1+T_{bs}) \dots} = 0$$

For a type 1 system,

$$K_v = \lim_{s \rightarrow 0} \frac{sK(1+T_1s)(1+T_2s) \dots}{s(1+T_{as})(1+T_{bs}) \dots} = K$$

For a type 2 or higher system,

$$K_v = \lim_{s \rightarrow 0} \frac{sK(1+T_1s)(1+T_2s) \dots}{s^J(1+T_{as})(1+T_{bs}) \dots} = \infty, \text{ for } J \geq 2$$

(43)

$$\therefore e_{ss} = \frac{1}{K_0} = \infty \text{ for type 0 systems}$$

$$e_{ss} = \frac{1}{K_0} = \frac{1}{K}, \text{ for type 1 systems}$$

$$e_{ss} = \frac{1}{K_0} = 0, \text{ for type 2 or higher systems}$$

### static Acceleration Error Constant $K_a$ :

The steady-state error of the system with a unit-parabolic input (acceleration input), which is defined by

$$e_{ss} = \lim_{s \rightarrow 0} \frac{s}{1 + G(s)H(s)} \cdot \frac{1}{s^3} = \frac{1}{\lim_{s \rightarrow 0} s^2 G(s) H(s)}$$

$$K_a = \lim_{s \rightarrow 0} s^2 G(s) H(s)$$

$$e_{ss} = \frac{1}{K_a}$$

For a type 0 system

$$K_a = \lim_{s \rightarrow 0} \frac{s^2 K (1+T_1 s)(1+T_2 s) \dots}{(1+T_a s)(1+T_b s) \dots} = 0$$

For a type 1 system

$$K_a = \lim_{s \rightarrow 0} \frac{s^2 K (1+T_1 s)(1+T_2 s) \dots}{s(1+T_a s)(1+T_b s) \dots} = 0$$

For a type 2 system

$$K_a = \lim_{s \rightarrow 0} \frac{s^2 K (1+T_1 s)(1+T_2 s) \dots}{s^2 (1+T_a s)(1+T_b s) \dots} = K$$

For a type 3 or higher system

$$K_a = \lim_{s \rightarrow 0} \frac{s^2 K (1+T_1 s)(1+T_2 s) \dots}{s^3 (1+T_a s)(1+T_b s) \dots} = \infty, \text{ for } J \geq 3$$

(44)

1&lt;

$\therefore e_{ss} = \infty$ , for type 0 and type 1 systems

$$e_{ss} = \frac{1}{K}, \text{ for type 2 systems}$$

$$e_{ss} = 0, \text{ for type 3 or higher systems}$$

type	$K_p$	$K_v$	$K_a$	$e_{ss}$ step	$e_{ss}$ Ramp	$e_{ss}$ Parabolic
0	$K$	0	0	$\frac{1}{1+K}$	$\infty$	$\infty$
1	$\infty$	$K$	0	0	$\frac{1}{K}$	$\infty$
2	$\infty$	$\infty$	$K$	0	0	$\frac{1}{K}$
3	$\infty$	$\infty$	$\infty$	0	0	0

Table -  $K_p, K_v, K_a$ , and steady-state error in terms of Gain  $K$ .

## Definitions of Transient - Response Specifications

- ① - Delay time  $t_d$  : The delay time is the time required for the response to reach half the final value the very first time.
- ② - Rise time  $t_r$  : The rise time is the time required for the response to rise from 10% to 90% of its final value.
- ③ - Peak time  $t_p$  : The peak time is the time required for the response to reach the first peak of the overshoot.
- ④ - Maximum (percent) overshoot  $M_p$  : The maximum overshoot is the maximum peak value of the response curve measured from unity.

$$\text{Maximum percent overshoot} = \frac{C(t_p) - C(\infty)}{C(\infty)} \times 100\%$$

- ⑤ - Settling time  $t_s$  : The settling time is the time required for the response curve to reach and stay within a range about the final value of size specified by absolute percentage of the final value (usually 2% or 5%).

(46)

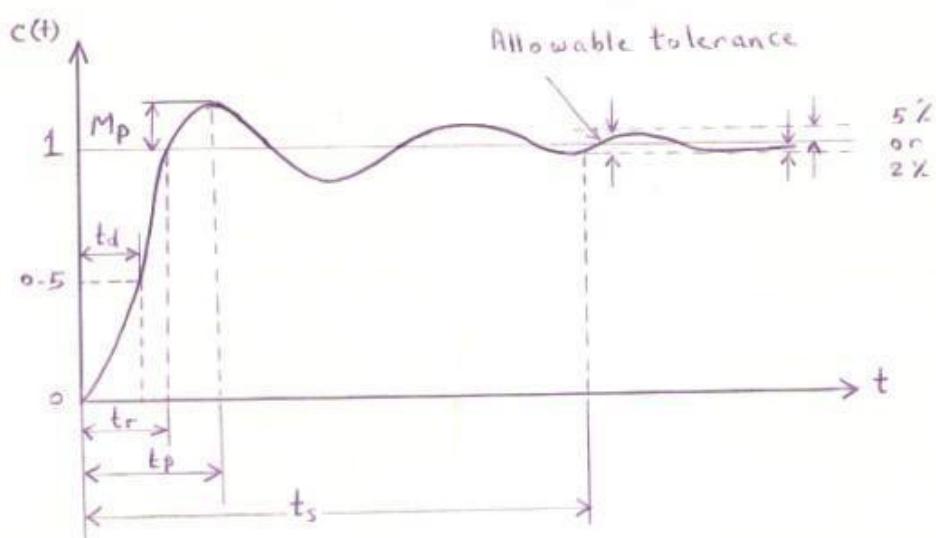


Fig. Unit-step response curve showing  $t_d$ ,  $t_r$ ,  $t_p$ ,  $M_p$ , and  $t_s$ .

In the Following, we shall obtain the rise time, peak time, maximum overshoot, and settling time of the second-order system given by equation:

$$\frac{C(s)}{R(s)} = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

The system is assumed to be underdamped.

Rise time  $t_r$ : Referring to equation :

$$c(t) = 1 - e^{-\zeta\omega_n t} \left( \cos\omega_n t + \frac{\zeta}{\sqrt{1-\zeta^2}} \sin\omega_n t \right)$$

We obtain the rise time  $t_r$  by letting  $c(t_r) = 1$

$$c(t_r) = 1 = 1 - e^{-\zeta\omega_n t_r} \left( \cos\omega_n t_r + \frac{\zeta}{\sqrt{1-\zeta^2}} \sin\omega_n t_r \right)$$

Since  $e^{-\zeta\omega_n t_r} \neq 0$ , we obtain

$$\cos\omega_n t_r + \frac{\zeta}{\sqrt{1-\zeta^2}} \sin\omega_n t_r = 0$$

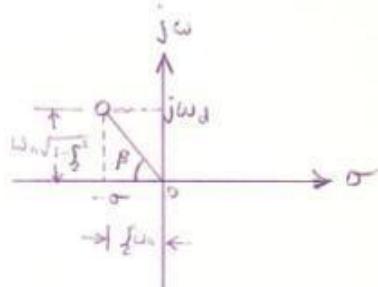
(47)

10

$$\text{or } \tan \omega_d t_r = -\frac{\sqrt{1-\frac{l^2}{\sigma^2}}}{\frac{l}{\sigma}} = -\frac{\omega_d}{\sigma}$$

$$\therefore t_r = \frac{1}{\omega_d} \tan^{-1} \left( \frac{\omega_d}{\sigma} \right)$$

$$t_r = \frac{\pi - \beta}{\omega_d}$$



Peak time  $t_p$ : Referring to equation:

$$\begin{aligned} c(t) &= 1 - e^{-\frac{l}{2}\omega_n t} \left( \cos \omega_d t + \frac{l}{\sqrt{1-\frac{l^2}{\sigma^2}}} \sin \omega_d t \right) \\ \frac{dc(t)}{dt} &= \frac{l}{2}\omega_n e^{-\frac{l}{2}\omega_n t} \left( \cos \omega_d t + \frac{l}{\sqrt{1-\frac{l^2}{\sigma^2}}} \sin \omega_d t \right) + \\ &\quad + e^{-\frac{l}{2}\omega_n t} \left( \omega_d \sin \omega_d t - \frac{l\omega_d}{\sqrt{1-\frac{l^2}{\sigma^2}}} \cos \omega_d t \right) \\ \left. \frac{dc(t)}{dt} \right|_{t=t_p} &= (\sin \omega_d t_p) \frac{\omega_n}{\sqrt{1-\frac{l^2}{\sigma^2}}} e^{-\frac{l}{2}\omega_n t_p} = 0 \end{aligned}$$

$$\sin \omega_d t_p = 0$$

$$\text{or } \omega_d t_p = 0, \pi, 2\pi, 3\pi, \dots$$

Since the peak time corresponds to the first peak overshoot:

$$\omega_d t_p = \pi$$

$$\text{hence } t_p = \frac{\pi}{\omega_d}$$

(48)

Maximum overshoot  $M_p$ :

The maximum overshoot occurs at the peak time or at  $t=t_p = \frac{\pi}{\omega_n}$ .

Assuming that the final value of the output is unity.

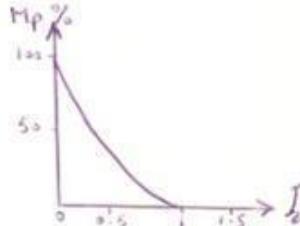
$$M_p = c(t_p) - 1 = -e^{-\frac{1}{2}\omega_n t_p} \left( \cos \pi + \frac{1}{\sqrt{1-\xi^2}} \sin \pi \right)$$

$$= e^{-\frac{1}{2}(\frac{\pi}{\omega_n})} = e^{-\frac{1}{2}(\frac{\pi}{\sqrt{1-\xi^2}})}$$

$$\text{The maximum percent overshoot is } e^{-\frac{1}{2}(\frac{\pi}{\omega_n})} \times 100 \%$$

If the final value  $c(\infty)$  of the output is not unity, then

$$M_p = \frac{c(t_p) - c(\infty)}{c(\infty)}$$

Settling time  $t_s$ :

For an undamped second-order system, the transient response is obtained from equation:

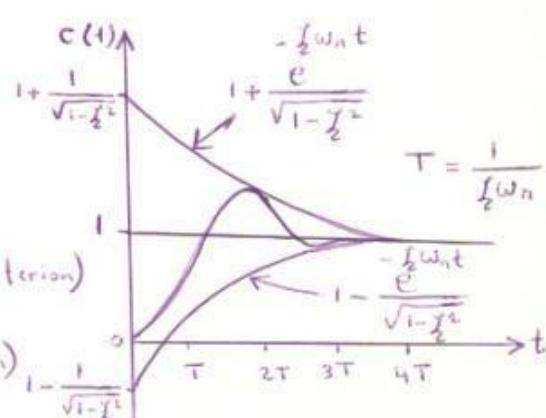
$$c(t) = 1 - \frac{e^{-\frac{1}{2}\omega_n t}}{\sqrt{1-\xi^2}} \sin\left(\omega_n t + \tan^{-1} \frac{\sqrt{1-\xi^2}}{\xi}\right), \text{ for } t \geq 0$$

The curves  $1 \mp \left( \frac{e^{-\frac{1}{2}\omega_n t}}{\sqrt{1-\xi^2}} \right)$

are the envelope curves of the transient response to a unit-step input.

$$t_s = 4T = \frac{4}{\sigma} = \frac{4}{\xi\omega_n} \quad (2\% \text{ criterion})$$

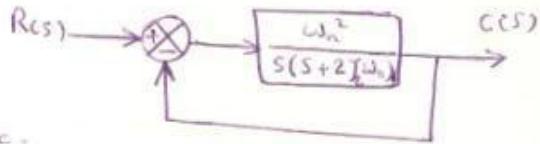
$$t_s = 3T = \frac{3}{\sigma} = \frac{3}{\xi\omega_n} \quad (5\% \text{ criterion})$$



(49)

VV

Ex: Consider the system shown in figure, where  $\zeta = 0.6$  and  $\omega_n = 5 \text{ rad/sec}$ .



Find  $t_r$ ,  $t_p$ ,  $M_p$ , and  $t_s$  when the system is subjected to a unit-step input.

Solution:

$$\omega_d = \omega_n \sqrt{1 - \zeta^2} = 5 \sqrt{1 - (0.6)^2} = 4$$

$$\sigma = \omega_n \zeta = (5)(0.6) = 3$$

$$\textcircled{1} \quad t_r = \frac{\pi - \beta}{\omega_d} = \frac{3.14 - \beta}{4}$$

$$\beta = \tan^{-1} \frac{\omega_d}{\sigma} = \tan^{-1} \frac{4}{3} = 0.93 \text{ rad}$$

$$\therefore t_r = \frac{3.14 - 0.93}{4} = 0.55 \text{ sec}$$

$$\textcircled{2} \quad t_p = \frac{\pi}{\omega_d} = \frac{3.14}{4} = 0.785 \text{ sec}$$

$$\textcircled{3} \quad M_p = e^{-\left(\frac{\sigma}{\omega_d}\right)\pi} = e^{-\left(\frac{3}{4}\right) \times 3.14} = 0.095$$

The maximum percent overshoot is thus 9.5 %

\textcircled{4} For the 2% criterion

$$t_s = \frac{4}{\sigma} = \frac{4}{3} = 1.33 \text{ sec}$$

For the 5% criterion

$$t_s = \frac{3}{\sigma} = \frac{3}{3} = 1 \text{ sec}$$