

Controlled Three Phase Half Wave Rectifiers

For RL Load

Let

$$V_{an} = V_m \sin \omega t$$

$$V_{bn} = V_m \sin(\omega t - 2\pi/3)$$

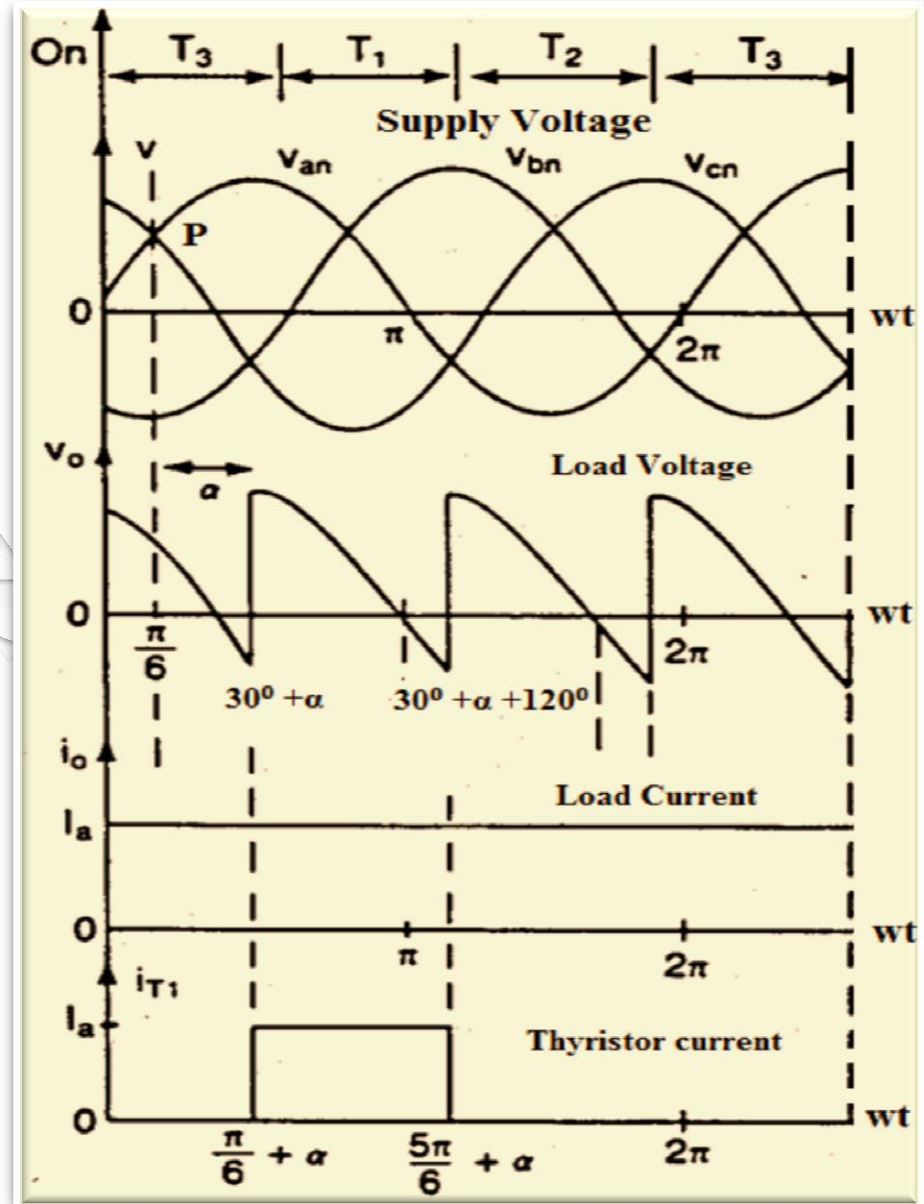
$$V_{cn} = V_m \sin(\omega t - 4\pi/3)$$

$$T_1 \text{ is triggered at } \omega t = \left(\frac{\pi}{6} + \alpha\right) = (30^\circ + \alpha)$$

$$T_2 \text{ is triggered at } \omega t = \left(\frac{5\pi}{6} + \alpha\right) = (150^\circ + \alpha)$$

$$T_3 \text{ is triggered at } \omega t = \left(\frac{7\pi}{6} + \alpha\right) = (270^\circ + \alpha)$$

Each thyristor conducts for 120° or $\frac{2\pi}{3}$ radians



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For RL Load

Load current is always continuous. The dc component of the output voltage is the average value, and load current is the resistor voltage divided by resistance.

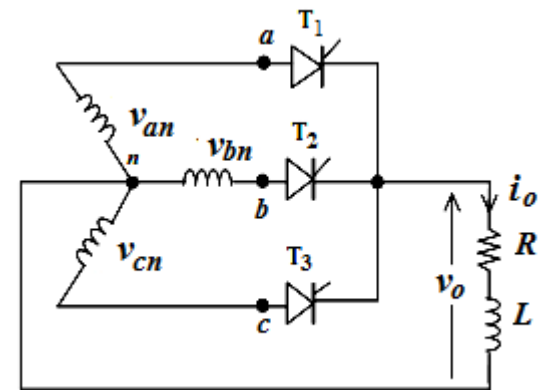
$$V_{dc} = \frac{3}{2\pi} \int_{\frac{\pi}{6}+\alpha}^{\frac{5\pi}{6}+\alpha} V_m \sin \omega t \, d\omega t = \frac{3\sqrt{3}V_m}{2\pi} \cos \alpha$$

$$I_{dc} = \frac{V_{dc}}{R} = \frac{3\sqrt{3}V_m}{2\pi R} \cos \alpha$$

The *rms* component of the output voltage and current waveforms are determined from

$$V_{rms} = \sqrt{\frac{3}{2\pi} \int_{\frac{\pi}{6}+\alpha}^{\frac{5\pi}{6}+\alpha} (V_m \sin \omega t)^2 d\omega t} = \sqrt{3}V_m \sqrt{\frac{1}{6} + \frac{\sqrt{3}}{8\pi} \cos 2\alpha}$$

$$I_{rms} = \frac{V_{rms}}{\sqrt{R^2 + (\omega L)^2}} = \frac{\sqrt{3}V_m}{\sqrt{R^2 + (\omega L)^2}} \sqrt{\frac{1}{6} + \frac{\sqrt{3}}{8\pi} \cos 2\alpha}$$



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For Resistive Load

In the case of a three-phase half wave controlled rectifier with resistive load, the thyristor T_1 is triggered at $\omega t = (30^\circ + \alpha)$ and T_1 conducts up to $\omega t = 180^\circ$. When the phase supply voltage decreases to zero, the load current falls to zero and the thyristor T_1 turns off. Thus T_1 conducts from $\omega t = (30^\circ + \alpha)$ to (180°) .

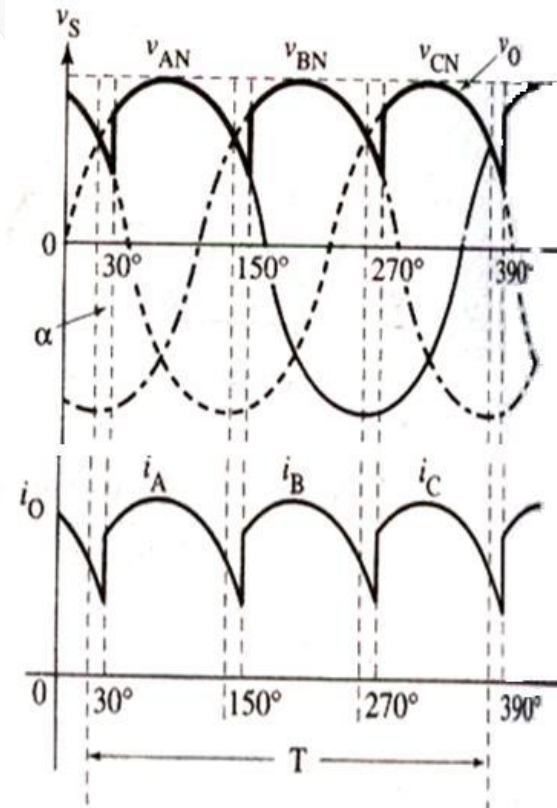
1- when $\alpha \leq 30^\circ$

$$V_{dc} = \frac{3}{2\pi} \int_{\frac{\pi}{6} + \alpha}^{\frac{5\pi}{6} + \alpha} V_m \sin \omega t \, d\omega t = \frac{3\sqrt{3}V_m}{2\pi} \cos \alpha$$

$$I_{dc} = \frac{V_{dc}}{R} = \frac{3\sqrt{3}V_m}{2\pi R} \cos \alpha$$

$$V_{rms} = \sqrt{\frac{3}{2\pi} \int_{\frac{\pi}{6} + \alpha}^{\frac{5\pi}{6} + \alpha} (V_m \sin \omega t)^2 d\omega t} = \sqrt{3}V_m \sqrt{\frac{1}{6} + \frac{\sqrt{3}}{8\pi} \cos 2\alpha}$$

$$I_{rms} = \frac{V_{rms}}{R} = \frac{\sqrt{3}V_m}{R} \sqrt{\frac{1}{6} + \frac{\sqrt{3}}{8\pi} \cos 2\alpha}$$



Controlled Three Phase Half Wave Rectifiers

For Resistive Load

2- when $\alpha \geq 30^\circ$

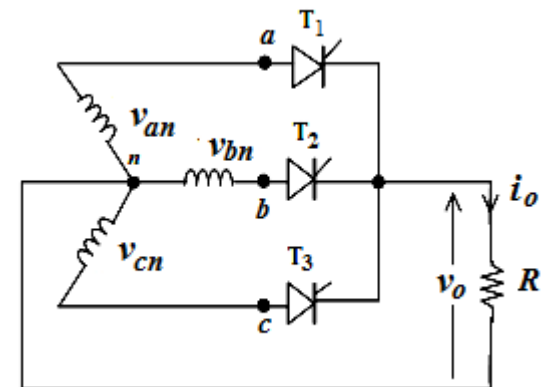
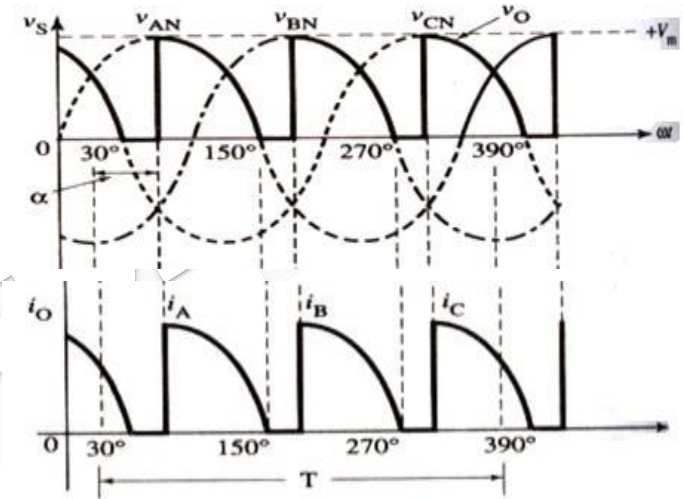
$$V_{dc} = \frac{3}{2\pi} \int_{\frac{\pi}{6} + \alpha}^{\pi} V_m \sin \omega t d\omega t = \frac{3V_m}{2\pi} (1 + \cos(\frac{\pi}{6} + \alpha))$$

$$I_{dc} = \frac{V_{dc}}{R} = \frac{3V_m}{2\pi R} (1 + \cos(\frac{\pi}{6} + \alpha))$$

$$V_{rms} = \sqrt{\frac{3}{2\pi} \int_{\frac{\pi}{6} + \alpha}^{\pi} (V_m \sin \omega t)^2 d\omega t} = \sqrt{\frac{3V_m^2}{4\pi} \int_{\frac{\pi}{6} + \alpha}^{\pi} (1 - \cos 2\omega t) d\omega t}$$

$$V_{rms} = V_m \sqrt{\frac{3}{4\pi} (\frac{5\pi}{6} - \alpha + \frac{1}{2} \sin(\frac{\pi}{3} + 2\alpha))} =$$

$$I_{rms} = \frac{V_{rms}}{R} = \frac{V_m}{R} \sqrt{\frac{3}{4\pi} (\frac{5\pi}{6} - \alpha + \frac{1}{2} \sin(\frac{\pi}{3} + 2\alpha))}$$



Controlled Three Phase Half Wave Rectifiers with Freewheeling Diode

